HF RADAR INSTRUMENTS, PAST TO PRESENT

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RADAR RETURNS FROM the ocean surface have been observed since the earliest days of radar. They were characterized as “clutter” because they often obscured targets, such as ships or aircraft. However, Crombie (1955) observed that some high-frequency (HF, 3–30 MHz) signals recorded near the sea had a distinctive Doppler shift of a fraction of a hertz above and below the transmitted signal. He correctly deduced that they were the result of Bragg scattering by ocean waves that were traveling radially toward or away from the radar and had a wavelength of one-half the radar wavelength. That observation launched the field that is now termed “radar oceanography,” the use of radar systems to study oceanographic properties.

Radar systems can be characterized by a number of parameters including operating frequency, geometry, platform, propagation mode, means of obtaining distance and angular resolution, etc. In the limited space of this paper only a few of the highlights of HF systems can be covered. For in-depth reviews, the reader is referred to articles by Croft (1972), Barrick (1978), and Shearman (1981, 1983).

Distance Measurement

Single pulse. The simplest means of determining distance is to use a short pulse of radar energy. The range resolution is given by ct/2 where c is the velocity of light, $3 \times 10^8$ m s$^{-1}$, and t is the pulse width in seconds. A disadvantage of this technique is that if the pulse is short to obtain good range resolution, the average power transmitted power is low and so is the resulting signal-to-noise ratio of the received signal, thus limiting the radar range.

Coded waveform. An alternative to a single pulse is a coded waveform. Figure 1 illustrates an 11-element Barker code used to observe two targets of unequal amplitudes. The radar transmits a sequence of short pulses coded so their autocorrelation function has a single, sharp central peak and low sidelobes. The range resolution is determined by the width of the individual pulses but the average power is raised by the number of pulses in the sequence. There are some limitations to this approach, however. If the sequence is too long, short-range targets cannot be seen because a portion of the echo arrives while the later part of the sequence is still being transmitted. (Most radars cannot receive signals while they are transmitting, because of severe overloading of the receiver.) Figure 1 also illustrates another problem of coded waveforms; there can be spurious responses (range sidelobes) from strong targets. Both of these prob-
lems can be reduced or eliminated by using more complicated waveforms, at the expense of additional data processing.

**FMCW.** Instead of transmitting short pulses, a radar can transmit a relatively long frequency-modulated (FM) continuous-wave (CW) signal as sketched in Figure 2. If the transmitted frequency is linearly swept and used as a reference for the received signals, a target at a particular range will produce a constant difference frequency whose value depends on its distance; more distant targets will produce higher frequencies. By analyzing the frequency content of the returned signal, targets at various ranges can be discerned. For most radars, the linear sweep is interrupted periodically to avoid overloading the receiver during reception of the echo.

**Doppler Measurement**

Doppler resolution, used to measure the velocity of the target, is obtained by repeating the range measurements, whether single pulse, coded waveform, or FMCW, at a regular rate and performing a time-series analysis on the samples obtained from each individual range measurement. A coherent integration time of $T_s$ provides a frequency resolution of roughly $\Delta f = 1/T$ Hz. The target velocity resolution, in turn, is given by $\Delta v = \lambda \Delta f/2$ m s$^{-1}$, where $\lambda$ is the radar wavelength in meters.

**Azimuth Angle Measurement**

Because of the long wavelengths involved, HF radars do not physically move antennas to look in different directions. Rather, they control the direction to which they are sensitive electronically using a variety of techniques.

**Phased array.** Conceptually, the simplest antenna system is a phased array of identical receiving elements spaced no more than $\lambda/2$ apart (to avoid severe sidelobes) with the line of the array perpendicular to the center of the desired set of beam directions. The beam is steered by adjusting the amplitude and phase of the signals from each of the elements and adding these signals coherently. The phase adjustment can be done using physical devices (coaxial cables, phase-shift networks, etc.) or digitally in the data processing after the signals from each element have been separately recorded. The angular resolution that can be obtained from an array with a total aperture of $D$ is roughly $\lambda/D$ radians. To obtain an angular resolution of $5^\circ$ (0.1 radian), an aperture of $10\lambda$ is required. In practice, it may not be possible to obtain enough area on a beach for this resolution, particularly at frequencies below 10 MHz.

**Synthetic aperture.** At the low end of the HF spectrum, it is impractical to obtain any appreciable directivity with a physical aperture. However, it is possible to use a technique borrowed from satellite technology, synthetic aperture. A simple antenna, for example, a loop or short whip, is carried along a straight line at a constant velocity that is less than the phase velocity of the Bragg-resonant ocean waves. The motion of the antenna spreads a narrow Bragg line into a band of direction-dependent frequencies, and Fourier analysis of the signals can yield their direction of arrival if it is assumed that currents are insignificant compared with the phase velocity of the Bragg waves. This technique works best at low frequencies (2 MHz, $\lambda = 150$ m) and apertures of up to 2 km have been synthesized this way (Tyler et al. 1974; Shearman 1981).

**Direction finding.** An alternative to the beamforming techniques is direction finding. The signals from two or more relatively closely spaced (Crombie 1972) or even co-located (Barrick et al., 1977) antennas are compared, either in phase or amplitude. This is done at each frequency bin in the analysis bandwidth. With $N$ antennas, it is possible to resolve at most $N-1$ directions at each frequency. A significant advantage of this technique is that the antennas are much smaller than in a phased array.

With all of these techniques, it is important that the amplitude and phase response of the antennas is very well known. Usually it is not sufficient to depend on ideal theoretical patterns or even electromagnetic modeling programs. Antenna-ground planes, cables, buried conductors, fences, and finite ground conductivity all contribute to the antenna patterns and ultimately they must be measured, usually with a portable signal source or a transponder. As the desired directivity

![Fig. 1: Sketch of waveforms for a radar using an N-element Barker code. The transmitted waveform (Tx) is at the top, followed by individual returns from two discrete targets (T1, T2) of relative amplitude 1.0 and 0.5, their sum (Sum), and the cross-correlation function (XCor) between the received composite signal and the transmitted signal at the bottom. The two targets are clearly resolved.](image-url)
Another significant result from this experiment was a measure of the absolute value of the radar cross section of the ocean.

Wave Measurements

Early wave measurements were made using both monostatic (co-located transmitter and receiver) and bistatic (separated transmitter and receiver) geometries. Radars located on land and on ships, various antenna configurations, and surface wave and sky wave (ionospheric) radio propagation. Estimation of ocean wave parameters using surface-wave radars usually involves receiving first-order scattered signals from a wide range of angles and assumes that the sea is homogeneous over the area surveyed; sky-wave radars generally look in a narrow range of directions and make use of the second-order signals. A few key experiments are mentioned below.

Bistatic Geometry

In the late 1960s Allen Peterson of Stanford University collaborated with Walter Munk and Bill Nierenberg of the Scripps Institution of Oceanography to investigate techniques of using HF surface-wave radar to make oceanographic measurements over large areas. Under Office of Naval Research sponsorship, Peterson, C.C. Teague, and G.L. Tyler of the Radioscience Laboratory at Stanford began experiments along the northern California coast using Prof. Peterson’s weekend cottage at Sunset Beach (south of Santa Cruz) as a field site. These experiments led to the first HF radar measurements of directional wave spectra for ocean swell (Peterson et al., 1970). They employed a bistatic geometry, which made use of LORAN-A transmitters operating near 1.9 MHz. These transmitters, now removed from service, had a peak power of many hundreds of kilowatts and used short pulses, so they made an ideal transmitter for a radar system. By receiving the direct signal and echoes a few hundred kilometers from the transmitter, it was possible to map a portion of the ocean-wave directional spectrum to the received Doppler shift by assuming that the sea was homogeneous over the observation region and that currents were small (Teague, 1971). However, because of gaps in coverage of the ocean wave spectrum, other techniques were sought.

Synthetic Aperture

Steady state. Several experiments were performed using a synthetic aperture receiving antenna in conjunction with LORAN-A transmitters. For these experiments, a small antenna was carried on a vehicle traveling in a straight line at a constant velocity close to the transmitter so that the geometry was essentially monostatic. In an experiment at Wake Island, a small island in the trade winds region, the directional distribution of 77 m ocean waves was measured under fully developed conditions (Tyler et al., 1974). The directional distribution was found to be consistent with a cos^s(θ/2) form, with s in the range of 2–12, and with a small pedestal to account for ~1% of the wave energy traveling upwind. Another significant result from this experiment was a measure of the absolute value of the radar cross section of the ocean (Teague et al., 1975). This measurement was made by observing the ratio of the echo energy to the direct energy from the transmitter a few kilometers from the receiver. Similar experiments were performed in the United Kingdom by Shearman et al. (1979) using a former LORAN-A transmitter in Wales.

Wave growth and shadowing. An experiment complementary to Wake Island was performed at Galveston, TX, along a long straight coastline (Stewart and Teague, 1980). Observations were made after the wind had shifted from onshore to offshore and the wave growth with distance and time was measured, again using a nearby LORAN-A transmitter. In Southern California wave shadowing by San Clemente and San Nicholas Islands was reported by Vesecky et al. (1980).

Phased Array

A dual-frequency phased-array radar was operated on the French Mediterranean coast by the University of Toulon (Broche, 1979) and used to estimate the significant wave height H_1/3, dominant wave frequency, and wind direction. A similar radar was used by the Institut Français du Petrole in the Shetland Islands (Shearman, 1983). A multifrequency radar constructed at Stanford Univer-
sity was operated on a ship during the 1978 Joint Air-Sea Interaction (JASIN) experiment (Teague, 1986). Although the emphasis in this issue is on surface-wave propagation, several sky-wave phased-array radars employing very narrow beam widths have been used. Maresca and Georges (1980) describe the 2.5 km Wide Aperture Research Facility (WARF) operated by SRI International, and Georges and Harlan (1994) describe the use of military surveillance radars to obtain oceanic winds.

**Direction Finding**

In an early experiment Crombie et al. (1970) and Crombie (1972) used a multifrequency coherent radar with a pair of phased-receiving whip antennas to observe the growth of wave energy offshore of Barbados. Using one antenna in a nondirectional mode, Crombie also observed small but significant wave energy traveling in opposition to the wind (Crombie et al., 1978). Direction-finding systems usually are used to measure currents rather than waves, as discussed in the next section.

**Wind Measurements**

Although HF radars do not directly respond to the wind, several researchers have estimated the direction and, in some cases, the speed of winds near the ocean surface by examining the signals scattered by the ocean waves raised in response to the wind. Long and Trizna (1973) used radar at Chesapeake Bay to map winds in the North Atlantic, and Stewart and Barnum (1975) evaluated the accuracy of that technique. Shearman and Wyatt (1982) describe the results of mapping winds during the JASIN experiment. Recent results from an experiment conducted at Duck, NC in 1994 show wind direction maps obtained with OSCR (Fernandez et al., 1997).

**Current Measurements**

Recently there has been considerable emphasis on mapping ocean currents. By examining the coherence between signals received on two closely spaced whips, Crombie (1972) observed that the phase of the coherence varied with Doppler frequency, implying that signals having different Doppler shifts were coming from different directions, and interpreted this as viewing a uniform current from different aspect angles. This result led to the development of the Coastal Ocean Dynamics Applications Radar (CODAR) (Barrick et al., 1977; Lipa and Barrick, 1983), which is the subject of several papers in this issue (Barrick and Lipa, 1997; Bjorkstedt and Roughgarden, 1997; Paduan and Cook, 1997). The CODAR system extends Crombie’s direction-finding array to a compact set of co-located antennas and thus requires very little beach space for operation. Phased-array radars have also been used to measure currents. Stewart and Joy (1974) used a multifrequency radar on San Clemente Island to measure the vertical current shear at two bearings. Ha (1979) used the multifrequency Stanford radar with a highly directional transmitting antenna to measure currents along its boresight and compared his measurements with drifting spar buoys. The same radar was used with a phased-array receiving antenna at Granite Canyon, south of Monterey, to study the effects of upwelling along the California coast (Fernandez, 1993; Shkedy et al., 1995; Fernandez et al., 1996). Maresca et al. (1980) examined tidal currents in the San Francisco Bay. Building on work by the CODAR, NOAA Wave Propagation Laboratory, and Stanford groups, a new array type HF radar system for the commercial market was developed by Marex Ltd., England. This radar, called Ocean Surface Current Radar (OSCR), uses a 16-element antenna array ~80 m long. OSCR instruments have been used for mapping tidal and residual surface currents along the coasts of Britain (Prandle, 1987). OSCR units have been sold in the United States: the Rosenstiel School of Marine and Atmospheric Science of the University of Miami used a pair of OSCR radars for coastal observations in a number of locations (Shay et al., 1995; Graber et al., 1996). A new multifrequency radar was constructed jointly by the University of Michigan, the Environmental Institute of Michigan, and Stanford and is in operation at Santa Cruz, CA.

**Conclusions**

Over the past 25 years HF radar systems have been used to measure the directional distribution of wave energy in the open ocean, the growth of waves offshore after a sudden change in wind direction because of a frontal passage, ocean current shear from a ship in the open ocean, and current and current shear from land-based locations. With proper calibration and data processing, HF radar is capable of providing wide-area measurements that are difficult or impossible to make any other way, and the radar data can provide useful supplements to conventional oceanographic measurements.

**References**


